Table V. Typical Test Data on Effect of Hydrogen-Shale Ratio on Product Distribution

Table V. Typical Test Data on Effect of Hydrogen-Shale Ratio on Product Distribution. Table V. Typical Test Data on Effect of Hydrogen-Shale Ratio on Product Distribution. Total shale charging time, 510 seconds Shale feed rate, 5.47 lb./hour. Hydrogen-shale ratio, 255% of stoichiometric. Total shale charging time, 510 seconds 1000 1000 1000 1000 1000 1000 1000 1											
Table V. Typical Test Do	ata on Em	ecrorn	yarogo		. Tota	al shale c	harging t	ime, 510	seconds		2 502
Shale feed rate, 5.47 lb./hour. Hydro Time of sampling, sec. Temp. at final center of shale, ° F. Temp. at bottom of shale, ° F. Temp. at bottom of inerts, ° F. Feed hydrogen rate, SCF/hr. Feed hydrogen space velocity, SCF/cu. fthr.	30 1349 1350 1407 88.6 10,030 88.1 0.0088	80 1310 1298 1412 88.6	150 1290 1290 1420 88.6	250 1308 1298 1430 88.6	350 1220 1246 1440 88.8	450 1235 1266 1450 89.0 4840	550 1273 1299 1458 89.0 4500	600 1280 1302 1450 89.4 4520	1310 1445 89.8 4540	800 1306 1326 1436 90.2 4560 82.9	1000 1350 1364 1435 90.4 4570 82.5 0.0198
Exit gas rate, SCF/hr. Total bed volume, cu. ft. Exit gas composition, mole % N2 CO CO2 H2 CH4 C2H6 C2H4 C3H6 Acetylene Benzene	0.0088 0 0.09 99.75 0.10 0.06 100.00	0.01 1.20 0.24 81.67 11.54 4.95 0.21	0.70 1.60 0.20 80.44 12.37 4.45 0.05 0.07 0.01 0.11	0.40 2.90 0.33 78.06 13.77 4.27 0.09 0.01 0.17	0.53 3.10 0.46 77.31 14.27 4.05 0.08	0.46 3.30 0.57 76.66 14.74 3.93 0.07	3.60 0.62 75.71 15.47 3.95 0.09	3.10 0.46 92.39 2.75 0.45 0.02	2.30 0.32 93.91 2.51 0.23 0.01	1.50 0.19 94.81 2.80 0.15	1.14 0.09 95.53 2.97 0.11
Total	0.006					0.636	0.655	0.101	0.082	0.084	
Conversion of organic carbon fed carbon, lb./lb. organic carbon in products, % As gaseous hydrocarbons As liquids As solid residue Total		2.9 × 2.9 × 3.4 ± 3	5 x Y + 3 P + 2 P	100 P		. v · . · ·			# # (5) # # (4) # (4)(6)		70.9 16.9 8.5 96.3

velocity above 5000 SCF/cu. foot-hour was primarily the result of increased linear velocity of the rapidly formed intermediate reaction products. Backmixing effects were found to be negligible over most of the range of flow rates studied (5).

Effect of Hydrogen-Shale Ratio on Product Distribution. In view of the important effect of the hydrogen-oil shale feed ratio on product distribution, the semiflow techniques were

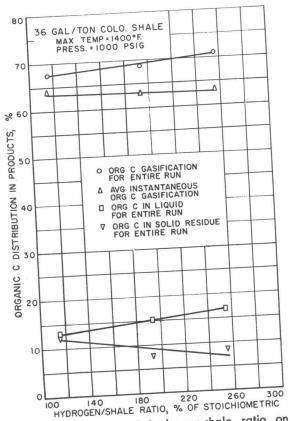
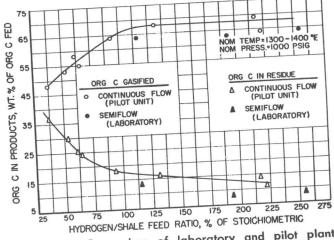


Figure 11. Effect of hydrogen-shale ratio on carbon distribution in products and average instantaneous carbon gasification

modified to permit control of this variable. Initially, small batches of oil shale were fed at frequent intervals onto a fixed bed of inerts. Results still showed an apparent effect of feed ratio above 100% of the stoichiometric requirements for conversion of the organic matter to methane, which was unexpected on the basis of oil hydrogasification results (10, 12, 13). However, these tests showed the expected negligible effect of an increase in total pressure from 1000 to 2000 p.s.i.g.

Further tests at 1200° to 1400° F. and 1000 p.s.i.g. were then conducted with a continuous feeding system in which oil shale was charged at a nearly constant rate for 510 seconds, corresponding to an average oil shale residence time of about 5 minutes. Thus, the hydrogen flow rate increased linearly with hydrogen-oil shale ratio. Typical test data are shown in Table V. As shown in Figure 11, instantaneous organic carbon gasification at hydrogen-oil shale feed ratios ranging from about 100 to 250% of stoichiometric remained nearly constant and averaged 63 to 64%. Total organic carbon gasification measured during the 1000- to 1100-second run



Comparison of laboratory and pilot plant Figure 12. test results

period was about 70%. The organic carbon distribution in the residue and the aromatic liquid products was about 13% each, at the lowest gas rate. The organic carbon in the residue decreased with an increase in hydrogen feed rate, as would be expected. All yield and organic carbon distribution data are uncorrected for low carbon balances (92 to 96%).

Higher conversions to gaseous hydrocarbons could, of course, be obtained by increasing oil shale residence times, although the maximum would be about 85 to 90%, since a minimum yield of aromatic liquids of 10 to 15% would be expected from previous experience in hydrogasification of petroleum hydrocarbons similar in composition to kerogen (10, 12, 13).

These test results have been verified by pilot-plant-scale tests. Although the pilot plant test program has not yet been completed, preliminary results are given in Figure 12 along with part of those shown in Figure 11. Good agreement in the two sets of data is apparent. Complete results from the pilot plant test program will be reported when the pilot plant test program is completed.

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